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The effect of deep unloadings on fracture toughness was examined for a HSLA ASTM A710 steel where toughwas examined for a noin noin noise while tought hess was evaluated in the elastic plastic regime by the J_R curve test method. During the J_R curve evaluated the $J_$ the J_R curve test method. During the J_R curve evaluation following modes were applied: (1) occasional full unloadings (P_{min} = 0); (2) occasional unloadings with compression to full closure of the loadings with compression to full closure of the loading with compression with the loading with the lo line displacement (V = 0; P_{min} < 0). The resulting J_R curves were compared with J_R curves generated for specimens tested in a standard procedure. Raising the J_R curve was judged as an increase in toughness and lowering it as a decrease.

INTRODUCTION

During standard J-integral fracture mechanics characterization tests a very careful load history is utilized. First the specimen tests a very careful load history is deflized. This specimen is fatigue precracked at a low cyclic stress level and the specimen is then tested by a number of small elastic unloadings. This load history is unlikely to be reproduced in actual load histories on

The objective of this work is to investigate effects of occa-The objective of this work is to investigate effects of occasional full unloadings ($P_{min} = 0$) and unloadings with compression to full closure of the load line displacement (V = 0; $P_{min} < 0$). the J_R resistance curves.

EXPERIMENTAL METHODS

The material used for the test program was a high strength low alloy steel (HSLA) which has an ASTM designation A710 grade A, class 3. The chemical composition for this material is presented in Table 1, and the mechanical properties are shown in Table 2. The specimens used were of 20% side grooved compact type (ITCT) with specimens used were of 20% side grooved compact type (fict) with cracks in the T-L orientation as defined by ASTM E 399 (1). The J_R curve tests were conducted at room temperature and in accordance

The results reported here utilized MTS-810 servo-hydraulic test with ASTM E 1152-87 (2). machine with PDP-11 mini computer. The computer used for calculamachine with FDF-11 milli computer. The computer used for calculation and storing data was Tektronix Model 4051. Typical load histories are shown in Fig. 1 and 2.

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Table 1 Chemical composition of HSLA steel A710 (wt %)

			mpobler						
C	Si	Mn	P	S	Ni	Cr	Мо	Cu	Nb
0.05	0.30	0.62	0.011	0.004	0.88	0.72	0.185	0.105	0.041

Tangila proporties of HSLA steel A710

Table 2 Tensile properties of fisha seed Arto										
Material	Yield strength	Tensile strength	Elongation	Reduction of						
	R _{00 2} (MPa)		% in 50 mm							
A710	645	730	27	73						

ANALYSIS OF THE RESULTS

To get J_R curves for presented load histories J-integral calculated according to the expression (1):

$$J_{(1)} = \frac{\left(K_1\right)^2 \left(1 - \nu^2\right)}{E} + J_{pl(1)}$$
where stress intensity factor, K_1 , is

$$K_{(1)} = [P_i/(BB_N W)^{1/2}]f(a_i/W)$$
 (2)

and plastic component of J is:

$$J_{p1(i)} = \left[J_{p1(i-1)} + \left(\frac{\eta_i}{b_i}\right) \frac{A_{p1(i)} - A_{p1(i-1)}}{B_N}\right] \left[1 - \frac{\gamma_i}{b_i}(a_i - a_{i-1})\right]$$
(3)

In Eq.3, for CT specimens, η = 2 + (0.522) b_1 /W, γ = 1 + (0.76) b_1 /W, where W -specimen width, b_1 -instantaneous length of remaining ligament, B_N -minimum specimen thickness, a_1 -instantaneous crack length and $A_{p1(1)} - A_{p1(1-1)}$ is the increment of plastic area under the load versus load-line displacement record between lines of constant displacement at points i-1 and i.

Crack lengths are determined using unloading compliance method (2). The resulting J_R curves, together with baseline J_R curve are shown in Fig. 3.

The first observation is that limited occasional number of full unloadings to nearly zero minimum loads (in this case 5) does not affect J_R curve which fall on the baseline J_R curve. On the other hand, occasional unloadings with compression to full closure of the load line displacement (V=O) lowered tear toughness on the subsequent tear steps, which is in agreement with the results of Joyce (3). In the same time, slope of the segments of such curve stayed parallel to the baseline J_R curve.

CONCLUSIONS

- 1. Conducted tests show complexity and problem of applicability of the J-integral as a characterization fracture parameter in the presence of the deep unloadings during the course of monotonic tearing.
- 2. Experiments showed that occasional unloadings with compression to full closure lower J_{R} curve, while full unloadings to $P_{\text{min}} \! = \! 0$ does not.

3. These results do appear to support the type of analysis proposed by Kaiser (4).

- (1) ASTM Standard E 399-79A, Test Method for Plane-Strain Fracture ADIRI Standard E 399-19A, Test method for riane-Strain fracture
 Toughness of Metallic Materials, Annual Book of ASTM Standards,
- Toughness of Metallic materials, Annual Book of Asir Standards, Part 10, 1987, pp. 540-561, Philadelphia.

 Part 10, 1987, pp. 540-561, Philadelphia.

 Determining JR Curves, Method for Determining JR Curves, Part 11, 1997, pp. 900-810. ADIM E1102-81, Standard lest method for Determining JR Cull Annual Book of ASTM Standards, Part 10, 1987, pp. 800-810,
- Annual Book of ASTM Standards, Part 10, 1987, pp.800-810,

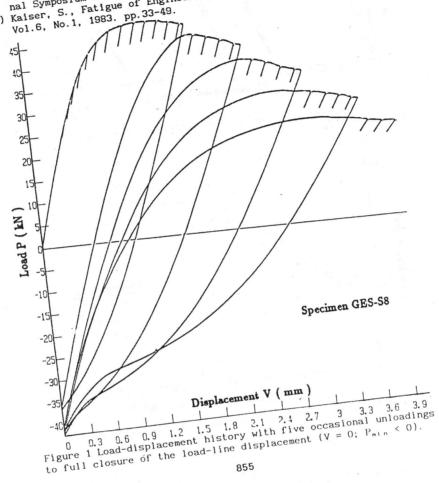
 Philadelphia.

 Development of a criterion for the effect on the standards, proceedings of the 16th Natio
 JR curve of elastic unloadings", Proceedings of the 16th Natio
 National Symposium of Fracture Mechanics, Boulder, Colorado, 1985.

 National Symposium of Engineering Materials and Structures,

 (4) Kaiser, S., Fatigue of Engineering Materials and Structures,

 Vol.6, No.1, 1983. pp.33-49.



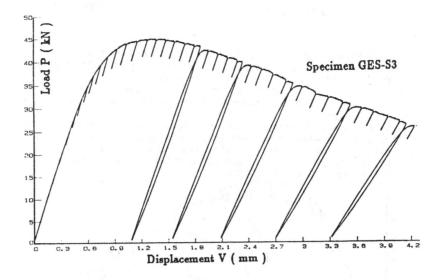


Figure 2 Load-displacement history with five occasional full unloadings ($P_{\text{min}} \, = \, 0$).

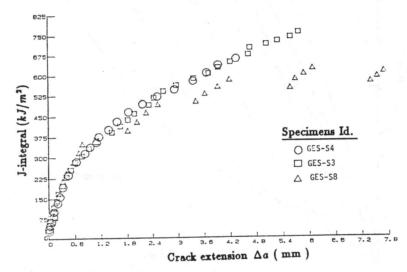


Figure 3 J_{R} curves for applied histories compared with baseline J_{R} curve.