Investigation of crack propagation in single optical fiber composite with thermal influence by finite element method

Ahanchian Mohammad
Ph.D. Candidate of Mechanical Engineering, De La Salle University

Arzumanyan Hovhannes, Verlinski Sergey
Assistant Professor of Department of Mechanics and Machine Sciences, State Engineering University of Armenia

ABSTRACT. Two parallel comparative ‘Conventional Method and Computer Simulation using ANSYS software’ for prediction of crack growth and its behavior in optical fiber are studied and presented in this work. Corresponding finite element analysis was performed to determine the evolution of stress and strain states. The method is developed and combined with the modified J-integral theory to deal with this problem. The effects of crack length, temperature and mechanical forces are investigated by Finite Element Method in the cracked body. The conditions where the Mode I stress intensity factor motivate fracture occurrence is investigated and variations of the different cases are discussed. The most deleterious situation is found to be that wherein the entire model reaches rupture at some stage. The accuracy of the method is investigated through comparison of numerical results with computerized simulation using commercial ANSYS software.

KEYWORDS. Crack propagation; Fracture; Temperature loading; Stress intensity factor; Breaking force.

INTRODUCTION

Recently, an increasing attention is attracted by a new development of microstructure optical fibers in telecommunication systems. An optical fiber is a single, hair-fine filament drawn from molten silica glass [1] which is widely used in communication systems. Optical fibers are going to be employed as a replacement of metal wires as the transmission medium in high-speed, high-capacity communication systems and are superior to that of conventional copper cable. In this design data is converted into light then transmitted via fiber optic cables with less loss. One of the most important usages of optical fibers is to transfer data sometimes in very long distances [2]. This duty could not be performed with physical failure and if the fiber core transpires fracture the data would not be transmitted properly. Since the main failure mode of fracture in optical fiber is mechanical fracture [3] more consideration is needed regarding the strength and associated reliability [4] of optical fibers which are major technical concerns before they can reach the full potential for telecommunication industry. Inevitable presence of sub micro cracks, flaws and hollows in the intersection of materials as a result of manufacturing and further processes [5] or on the surface of glass under either tension or bending [6] play a significant role for concentrating stress near the crack tip which decrease the strength of the material. Nevertheless, unfortunately, very few investigations have been conducted on their mechanical and fracture behavior of microstructure optical fibers [4]. These studies were conducted without considering temperature impacts. The goal of the current study is to investigate the fracture behavior of microstructure optical fibers containing surface cracks and environmental effects like temperature. Therefore, finite
element method is coded in MathCAD program to inspect fracture behavior and the results are compared with the ANSYS analysis. The effects of crack configurations, closure stresses and temperature on the failure load have also been investigated.

**CONSTITUTIVE MODEL OF OPTICAL FIBER**

The model of optical fiber is a composition of aluminum and silica glass as core which is developed within the framework of Small Static Displacement. The material properties are presented in Tab. 1. Two isotropic and homogeneous materials, joining to constitute a model of fiber optic in two-dimensional plane stress geometry with an initial circular crack on their meeting line are considered. According to the mentioned significance of optical fiber, ability of FEM and since computer modeling is useful to conduct virtual experiments with lower cost [7]; the authors decided to simulate a proper model on this design.

<table>
<thead>
<tr>
<th>Material</th>
<th>Density, Kg/m³</th>
<th>Modulus of Elasticity, MPa</th>
<th>Modulus of rigidity, MPa</th>
<th>Poisson’s Ratio</th>
<th>Thermal Conductivity, W/m.K</th>
<th>Thermal expansion, 1/C</th>
</tr>
</thead>
<tbody>
<tr>
<td>Glass</td>
<td>25400</td>
<td>46200</td>
<td>18600</td>
<td>0.245</td>
<td>6.21</td>
<td>8.00E-05</td>
</tr>
<tr>
<td>Aluminum</td>
<td>26600</td>
<td>71000</td>
<td>26200</td>
<td>0.334</td>
<td>237</td>
<td>2.36E-05</td>
</tr>
</tbody>
</table>

Table 1: Typical property of materials [8, 9].

The diameter of optical fiber as standard is assumed to be 125 µm having a circular crack in the intersection line of two materials. Three different cases considering crack lengths of 3.5, 7 and 10.5 µm are investigated. In the first situation, the crack has the smallest length that is in two dimensional polar coordinate \( r \) (radius of crack tip) is equal to the radius of core and \( \theta \) (angle between crack tip and X direction) had been assumed to be 15 degree. For other cases, radius had been kept constant and \( \theta \) had been incremented by 15 degree in order to increase crack length. The problem is investigated in Linear Elastic Fracture Mechanics (LEFM) with Plane stress approach. Due to symmetry of the problem, a quarter segment of the model is analyzed. Boundary conditions are imposed such as horizontal line is constrained in Y direction and vertical line is constrained in X direction; both lines are considered as symmetric along their direction. Applied forces are imposed in X any Y directions with constant values and the breaking forces are calculated for each case. Thermal condition is assumed to have constant value in each half of the quarter model, the lower part of quarter model has 50 °C and the upper part has 60 °C in order to have thermal gradient as presented in Fig 1.

![Figure 1: Applied forces and Thermal conditions on the model.](image-url)
CONVENTIONAL FRACTURE ANALYSIS

To numerically predict crack formation and growth of this model under accidental loading, it is necessary to characterize fracture properties at the microscopic level. To approach this objective a complete code of program using finite element method was written by the authors in MathCAD software. The geometrical characteristics, material properties and boundary conditions are attributed to the model. Corresponding finite element analysis was performed to determine the evolution of stress and strain states. For more comprehensible results and better facileness for comparison Von Misses stress had been calculated across the model using Eq. (1).

\[
\sigma_{eq} = \frac{1}{\sqrt{2}} \sqrt{\left(\sigma_x - \sigma_y \right)^2 + \left(\sigma_y - \sigma_z \right)^2 + \left(\sigma_z - \sigma_x \right)^2 + 6\left(\tau_{xy}^2 + \tau_{yz}^2 + \tau_{xz}^2\right)}
\]  

(1)

According to the theories in Fracture Mechanics, Stress Intensity Factor was calculated throughout the model and was applied to obtain J-integral. According to energy criterion, the critical energy release rate was determined and the crack extension was predicted and is presented in this paper. The breaking force values which lead the crack to propagate were obtained using Trial and Error Method for each case. The model will start propagation at low stresses and tends to extend at the tip of the crack [10, 11]. If the region be plastic at the tip of the crack, the metal mass around the crack would support the stress and the structure is not endangered [12]. Recent work on microstructure silica optical fibers indicated that they failed in a brittle manner and cracks initiated from the fiber surfaces [13]. According to the results, crack will propagate on the brittle area which is glass. The initiation and propagation of crack through brittle materials is at great speeds near the speed of sound [14]. Afterwards, thermal conditions were imposed and the complete procedure was done again. Based on the results, it is studied that crack will not growth anymore when the model is subjected to breaking force and thermal condition. Moreover, the largest crack needs less force to be broken. The contour plots for maximum crack length solved by MathCAD are presented in Fig. 2. Fig. 2.a shows Von Misses stress distribution subject to critical loading. Based on the data the highest amount of equivalent stress is placed near the crack tip. Fig. 2.b presents Von Misses stress distribution subject to critical loading and thermal conditions. It is shown that the maximum amount of equivalent stress is decreased after applying thermal conditions which prevents crack propagation and material failure. The approximation of crack propagation subject to critical loading is illustrated in Fig. 2.c.

The red region in Fig. 2.a shows the highest amount of equivalent stress. It is placed at the crack tip due to the fact that stresses concentrate at the crack tip. In Fig. 2.b the reduction of maximum amount of equivalent stress is a result of temperature. The prediction of crack propagation is presented by red region in Fig. 2.c. It shows that crack will propagate in silica that is a brittle material meaning that it fractures rather than deforming plastically. It responds to increasing mechanical load until a slow-growing microscopic crack exceeds a certain threshold at which point the crack grows rapidly and the material fractures [3].

Figure 2: Contour plots for maximum crack length (critical length), solved by MathCAD, (a) Von Misses stress distribution subject to critical loading, (b)Von Misses stress distribution subject to critical loading and thermal conditions, (c) Approximation of crack propagation subject to critical loading.
SIMULATION BY ANSYS

Consequently six different cases are discussed and each case is simulated by ANSYS to justify the accuracy of the written code in MathCAD. Some results are presented subsequently. The partial zoomed contour plots of ANSYS analysis of Von Misses stress distribution for the largest crack size subject to critical loading is presented in Fig 3.a. The result after imposing thermal condition to the previous situation is presented in Fig 3.b.

Figure 3: Zoomed contour plots for maximum crack length (critical length), simulated by ANSYS, (a) Von Misses stress distribution subject to critical loading, (b) Von Misses stress distribution subject to critical loading and thermal condition.

COMPARING THE RESULTS OF CONVENTIONAL METHOD AND ANSYS SIMULATION

In the first situation, the crack has the smallest length that is in two dimensional polar coordinate radius of crack tip is equal to the radius of core and the angle between crack tip and X direction had been assumed to be 15 degree. Critical force for this type of crack is -1.95 N; In this case maximum value for equivalent stress is 12.13 MPa, and is placed near the crack tip in Aluminum material. By adding thermal condition to applied force, maximum value for equivalent stress would be 12.02 MPa, which is lower than previous case.

Figure 4: Comparison of maximum Von Misses stress in different cases.
Maximum Von Misses stress and breaking force for different cases are presented in Tab. 2. The lowest amount of breaking force occurs in the largest crack size showing that we are near critical crack size. The value of stresses determine by conventional method and ANSYS simulation are presented and demonstrate that the differences are less than 1% which prove the accuracy of written code.

<table>
<thead>
<tr>
<th>Crack length, µm</th>
<th>Breaking Force, N</th>
<th>Mechanical Loading</th>
<th>Mechanical &amp; Thermal Loading</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>CM* MPa</td>
<td>ANSYS MPa</td>
</tr>
<tr>
<td>3.5</td>
<td>1.94</td>
<td>12.14</td>
<td>12.22</td>
</tr>
<tr>
<td>7</td>
<td>2.28</td>
<td>12.76</td>
<td>12.66</td>
</tr>
<tr>
<td>10.5</td>
<td>0.85</td>
<td>10.91</td>
<td>11.01</td>
</tr>
</tbody>
</table>

*CM: Conventional Method

Table 2: Maximum Von Misses stress distribution and breaking force for different cases.

**CONCLUSION**

The computational results presented in this research demonstrate the capabilities of the energy criterion towards modeling fracture in microstructure composites such as optical fiber. Critical forces in each case are obtained and it is clear that applying temperature condition would prevent the fracture process and fracture occurs under higher stresses as a result the optical fiber should be protected from low temperatures by adding cladding. It also protects from mechanical loading. Moreover, Prediction of crack branching and propagation is summarized and compared. The maximum stress magnitudes which instigate the crack are presented and compared. This shows that how big mechanical loading could our design withstand. Consequently, there are some parameters that mitigate crack propagation which are higher temperature, lower stresses and smaller grain size. This theory is a result of investigation by conventional method. When the temperature increases, a higher stress is required for a crack to propagate. Another point is that large crack size with 45 degree, is critical length and crack propagation occurs under minimum value of mechanical force and shows that production control should be improved properly.

**REFERENCES**